



A. Simulation of magnetizing process

Figure 2 shows a simulation model for the first step (magnetization analysis). A rotor consists of a Nd-Fe-B bonded ring magnet and a soft magnetic core made from silicon steels, and the ring magnet is arranged on the surface of the core. The inner and outer radii of the ring magnet are 23.4 mm and 25.15 mm, respectively. We placed the rotor in a magnetizer which consists of a silicon steel yoke and exciting coils, and applied a magnetization current of 44 kA·turn to the coils. Consequently, we obtained the magnetized ring magnet with 8 magnetic poles.

B. Determination of demagnetization curves at room and exposure temperature

After the magnetizing process, we determined the coercivity and the demagnetization curves of each element in the magnet. The coercivity of each element was determined individually based on the measured relationship between the coercivity and the maximum applied field (Fig. 3). The demagnetization curves were also determined individually based on the relationship between the demagnetization curves and the experienced maximum applied field (Fig. 4). For Magnet #2, both relationships were also obtained by the same measurements for Magnet #1.

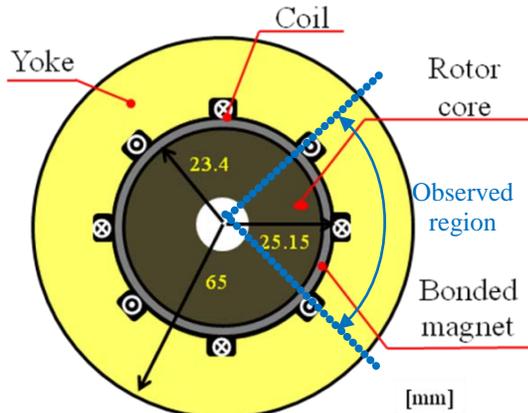


Fig.2 Simulation model used in the magnetization analysis. A rotor for a SPM motor and a magnetizer were modeled. The rotor consists of a Nd-Fe-B bonded ring magnet and a soft magnetic core made from silicon steels.

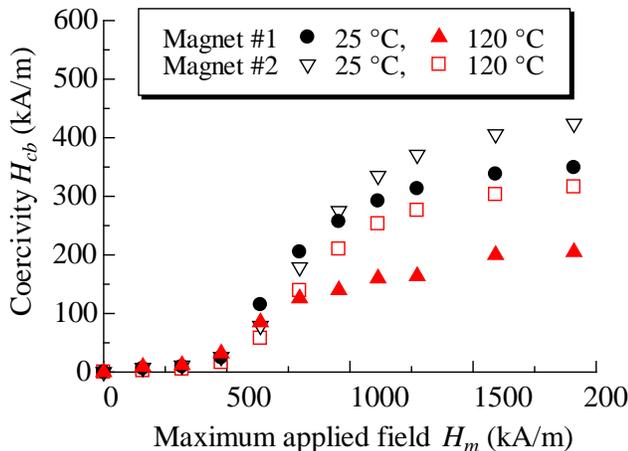
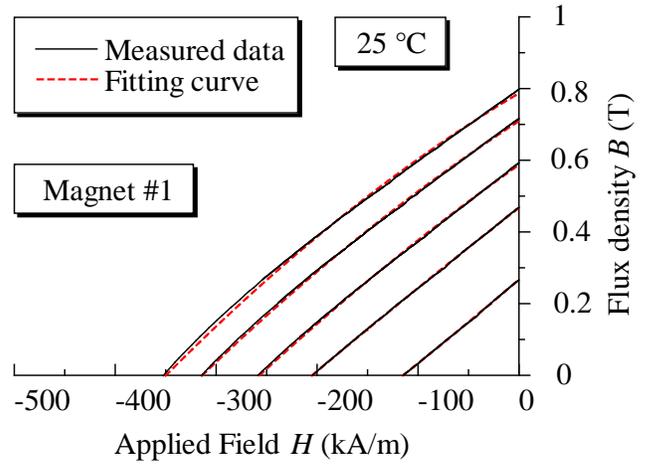


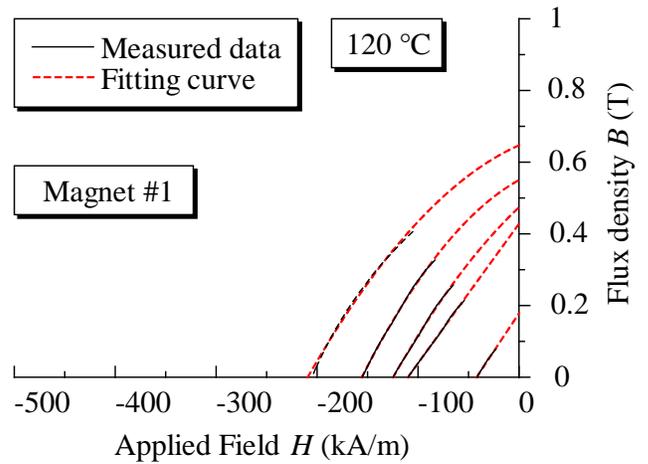
Fig.3 Relationships between the coercivity and the maximum applied field.

C. Simulation of distributions of magnetization at room and exposure temperature

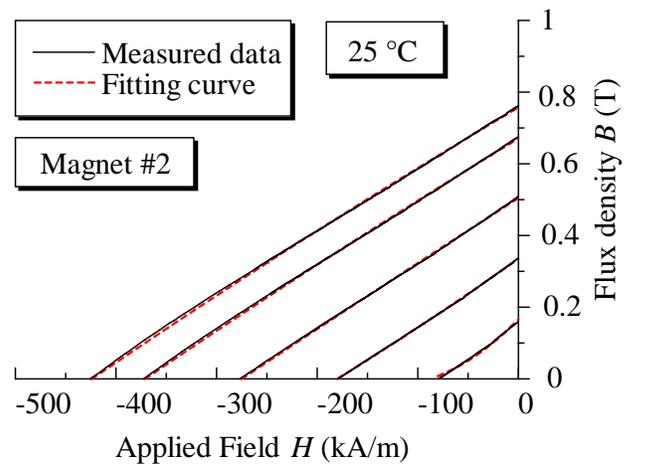
From the simulations of the steps 1 and 2, we obtained the values of the coercivity and the demagnetization curves of each element in the magnet. In this step, we defined the coercivity and the demagnetization curve to each element as material properties, and then carried out the FEM analysis of magnetic field. As a result, we obtained the distributions of the magnetization in the magnet.



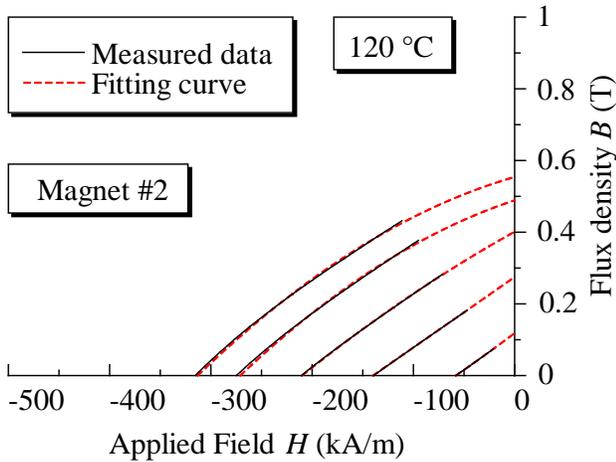
(a) Room temperature (25 °C)



(b) High temperature (120 °C)



(c) Room temperature (25 °C)



(d) High temperature (120 °C)

Fig. 4 Measured demagnetization curves of Magnet #1 and Magnet #2 at 25 °C and 120 °C. The fitting curves are also shown in this figure. The experienced maximum applied fields were 637, 796, 955, 1273, 1910 kA/m

D. Prediction of distribution of flux loss

The flux loss  $FL$  in the magnet is calculated by the following equation [3].

$$FL = \frac{1 - I_w(T_{ex})}{I_w(T_{RT})\{1 - \alpha(T_{ex} - T_{RT})\}} \quad (1)$$

Where  $I_w(T_{RT})$  and  $I_w(T_{ex})$  are the magnetizations at room temperature  $T_{RT}$  and the exposure temperature  $T_{ex}$ , respectively. The values of  $I_w(T_{RT})$  and  $I_w(T_{ex})$  obtained in the step 3 were used for the calculation of the flux loss.  $\alpha$  is a temperature coefficient of the magnetization, and the measured  $\alpha$  values of Magnet #1 and Magnet #2 are  $9.75 \times 10^{-4} \text{ K}^{-1}$  and  $9.36 \times 10^{-4} \text{ K}^{-1}$ , respectively.

III. RESULTS AND DISCUSSION

A. Flux loss in the ring magnet made from Magnet #1

Figure 5 shows the distribution of the flux loss and the demagnetizing field in the ring magnet made from Magnet #1. Since the simulation model has periodicity, we only showed the distributions for “Observed region” shown in Fig.2. As shown in Fig.5, large flux loss was observed in the inner side of the ring magnet, and the regions with large flux loss were correlated with the regions with large demagnetization field. This correlation agrees with the result for our previous study [4], [7], and suggests that we should pay attention to the regions with large demagnetization field to reduce in the flux loss.

B. Flux loss in the ring magnet with locally enhanced coercivity

It is well-known that a magnet with high coercivity has high thermal stability [8], [9]. Therefore, we considered that an enhancement of the coercivity in the regions with large demagnetization field is effective to reduce in the flux loss. In order to clarify the effect of the enhancement in the coercivity

on the reduction in the flux loss, we enhanced the coercivity in the ring magnet by partial replacement of inner side of Magnet #1 with Magnet #2, and evaluated the flux loss.

The thicknesses of Magnet #1 and Magnet #2 are 1.25 mm and 0.5 mm, respectively. The volume fraction of Magnet #2 in the ring magnet is approximately 8 vol.%. Figure 6 shows flux densities on the rotor surface for the ring magnets without or with locally enhanced coercivity. The angle from -45 to 45 degree corresponds to the angle of “Observed region” shown in Fig. 2. Both ring magnets showed almost the same waveforms of the flux density, and we confirmed that the flux density is not affected by the enhancement in the coercivity.

Figure 7 shows the distribution of the flux loss in the ring magnet (a) before and (b) after the enhancement in the coercivity. We confirmed that the enhancement in coercivity enables us to reduce in the flux loss in the ring magnet. The average value of the flux loss in the ring magnet with locally enhanced coercivity was 29.9 %, and this value was smaller than 37.5 % for the ring magnet without the enhanced coercivity.

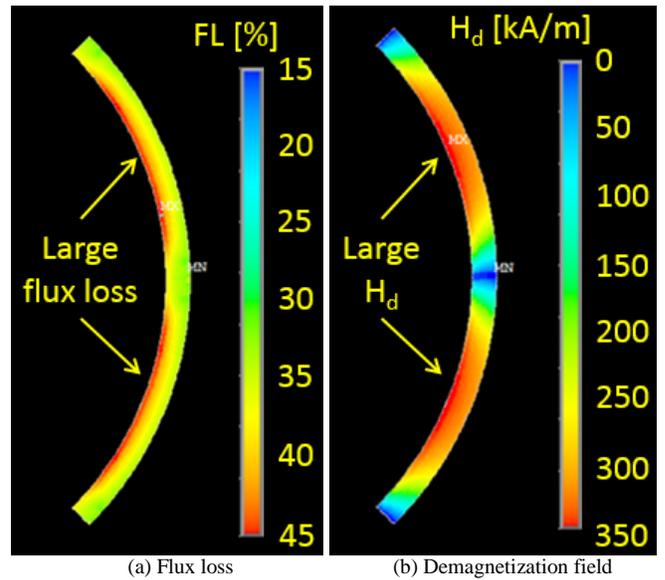


Fig.5 (a) Flux loss and (b) demagnetization field in the ring magnet made from Magnet #1.

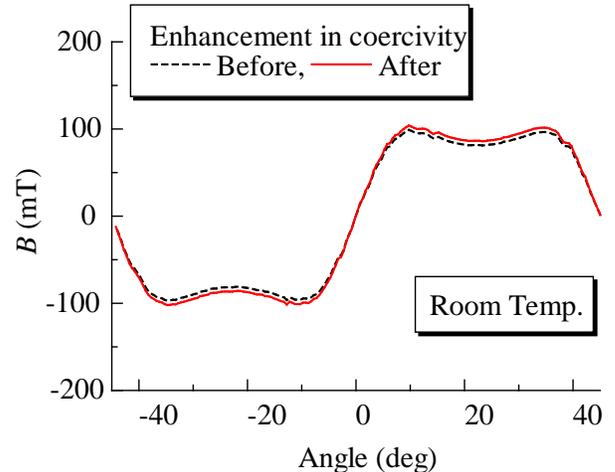


Fig.6 Flux densities on the rotor surface for the simulation models without or with locally enhanced coercivity in the ring magnet.

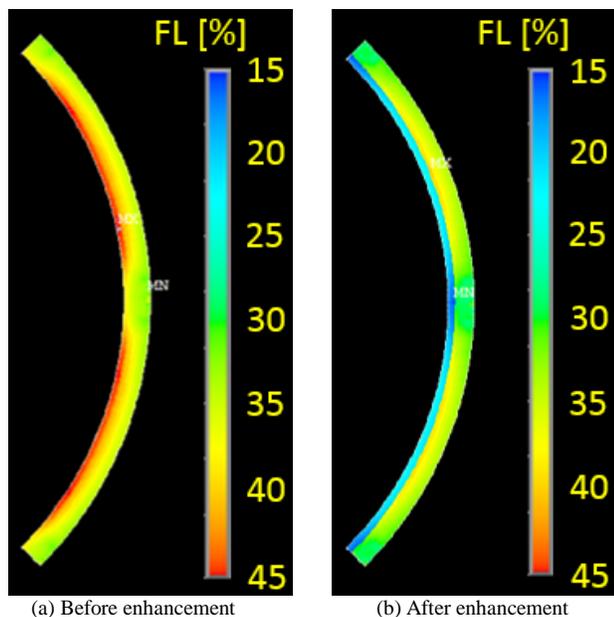


Fig.7 Flux loss in the ring magnet (a) before and (b) after the enhancement in the coercivity.

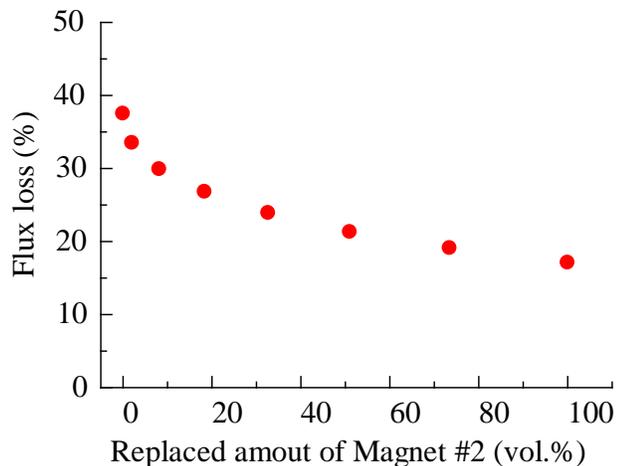


Fig.8 Flux loss of the ring magnet as a function of volume fraction of Magnet #2.

Figure 8 shows the flux loss of the ring magnet as a function of replaced amount of Magnet #2. The flux loss rapidly decreased by small replacement of Magnet #2, and we found that that large replacement isn't required for the reduction in the flux loss.

From above-mentioned results, we found that locally enhanced coercivity in a Nd-Fe-B bonded ring magnet for a SPM motor is one of hopeful methods to reduce in the flux loss.

#### IV. CONCLUSION

We applied our previously-proposed prediction method for the flux loss to a Nd-Fe-B bonded ring magnet for a SPM motor, and investigated the reduction in the flux loss of the ring magnet. The obtained results are summarized as follows;

- (1) Large flux loss was observed in the inner side of the ring magnet.
- (2) Demagnetizing filed was also, large in the inner side of the ring magnet, and this area a feels the flux loss.
- (3) Local enhancement in the coercivity of the ring magnet is effective to reduce in the flux loss strongly.
- (4) Large replacement of the bonded magnet with high coercivity isn't required for reduction in the flux loss.

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