Effect of tank shape on survival and growth of Pacific bluefin tuna *Thunnus orientalis* larvae

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Abstract 21

22 We examined the effect of rearing tank shape on survival and growth of Pacific bluefin tuna *Thunnus orientalis* larvae. Cylindrical $(1.7 \times 10^3 \text{ cm}^2 \text{ water surface area; } 30 \text{ cm deep})$ 23 and rectangular $(1.8 \times 10^3 \text{ cm}^2 \text{ water surface area}; 28 \text{ cm deep})$ tanks (n=3 each) were filled 24 with 50 liters of seawater. One air stone with a 100 ml/min aeration rate was set at the 25 bottom center of each tank. Light intensity at the water surface was 2000 lux with a 26 photoperiod of 24L:0D. Larvae were introduced into each tank at a rate of 10 individuals/l 27 at 2 days post-hatching (dph). Rotifers were fed at 10 individuals/ml and their distribution 28 in tanks was measured. Survival of larvae in cylindrical tanks (CT; 52.7±5.1%) at 8 dph 29 was higher than that in rectangular tanks (RT; $0.8\pm0.7\%$, p<0.01). Meanwhile, larvae 30 growth was not significantly different between tank shapes either in body length (CT: 31 32 4.23±0.26 mm; RT: 4.09±0.20 mm) or dry weights (CT: 95.1±17.6 μg; RT: 67.7±10.9 μg). 33 The swimbladder inflation rate of larvae also did not differ significantly between tank shapes (CT: 16.5±14.5%; RT: 56.9±3.47%). Rotifer distribution was higher at tank 34 35 bottom in both shapes (p < 0.05). Two-phase bubbly flow simulations in the tanks revealed that the low-flow area was larger in the RT. The low-flow area at tank bottom varied by 36 37 tank shape, occurring at the edge of the tank wall on the bottom in the CT, and from the center of the tank (air stone) to the tank wall in the RT. These low-flow areas at tank 38 bottom coincided with areas of higher rotifer distribution, which may be a cause of 39 sinking syndrome in fish larvae. Our results indicate that small-scale (50-1) PBT 40 larviculture experiments can be conducted using a CT with the present aeration system, 41 42 and that an RT requires an improved aerator in place of the single air stone.



Keywords: Pacific bluefin tuna; rearing tank shapes; sinking syndrome; survival; flow

44 field

45 **1. Introduction**

Pacific bluefin tuna (PBT) *Thunnus orientalis* is a commercially important fish in Japan, 46 Korea, Taiwan and the United States (Craig et al., 2017). Aquaculture for PBT utilizes 47 wild-caught juveniles as seedlings (Ottolenghi, 2008), and overfishing of PBT juveniles 48 has led to a decline of the PBT population in the wild (Craig et al., 2017). Recently, the 49 50 full life cycle of PBT was successfully completed under aquaculture conditions for the increasing demands of PBT seedlings (Sawada et al., 2005). However, high mortality 51 occurred during the first 10 days post-hatching (dph), followed by cannibalism during the 52 late larval and juvenile stages, and high mortality occurred by collision with tank or net 53 54 walls during the juvenile stage (Sawada et al., 2005). The high mortality during the first 10 days is an obstacle that must be solved for mass production of *Thunnus* species to gain 55 a stable large-scale supply of seedlings (Woolley et al., 2013; Nakagawa et al., 2011; 56 Sawada et al., 2005). 57

The sinking syndrome is a main cause of high mortality during the early larval 58 stages in PBT larviculture (Masuma et al., 2011). This occurs when larvae sink to the 59 60 bottom during dark periods because larval swimming activity is low at night, and their body density is higher than that of seawater (Nakagawa et al., 2011; Tanaka et al., 2009; 61 Takashi et al., 2006). Sinking syndrome occurs in many marine fish larvae, including the 62 striped trumpeter Latris lineata (Trotter et al., 2005), greater amberjack Seriola dumerili 63 (Teruya et al., 2009), yellowtail kingfish S. lalandi (Woolley and Qin, 2013), leopard coral 64 grouper *Plectropomus leopardus* (Takebe et al., 2011), kelp grouper *Epinephelus bruneus* 65 (Ching et al., 2014) and tiger grouper E. fuscoguttatus (Ching et al., 2016). Sinking 66 syndrome can be reduced by increasing the aeration rate at night (Tanaka et al., 2018; 67 Nakagawa et al., 2011) and/or creating conditions in which the larvae are suspended 68

within the water column of the rearing tank (Kurata et al., 2017; Ching et al., 2016, 2014;
Takebe et al., 2011; Tanaka et al., 2009) and by continuous illumination (Kumon et al.,
2018; Kurata et al., 2017).

72 In PBT larviculture, water temperature (Tanaka et al., 2018), aeration rates (Tanaka et al., 2018; Kurata et al., 2017; Nakagawa et al., 2011) and light conditions 73 74 (Kurata et al., 2017) have been studied as physical environmental factors that affect sinking syndrome in PBT larvae. However, information on the effects of tank shape, 75 which affect the early survival of marine fish larvae (Ruttanapornvareesakul et al., 2007) 76 are lacking. In the present study, we hypothesized that tank shape may affect the survival 77 and growth of marine fish larvae. To examine this possibility, we conducted larviculture 78 experiments in small 50-l tanks of different shapes. We chose a cylindrical tank (CT) with 79 axisymmetrical flow field patterns (Sumida et al. 2013), and a rectangular tank (RT) with 80 three-dimensional (3-D) complicated flow field patterns (Takakuwa et al., 2018), to 81 82 investigate the effect of tank shape on survival and growth of PBT larvae. We also examined the distribution of rotifers to estimate the flow field in tanks, and visualized the 83 84 flow fields by simulation.

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86 2. Materials and Methods

Three blue plastic CT (46 cm in diameter) and blue acrylic RT (60 cm \times 30 cm \times 35 cm depth) with a 50-1 working volume were used in this study. The aspect ratio (liquid depth/internal radius of the tank) of the CT was 1.3. We assumed that the aspect ratio of the RT was also 1.3, since the water surface area and depth of the RT (1.8 \times 10³ cm² \times 28 cm) were almost equal to those of the CT (1.7 \times 10³ cm² \times 30 cm). Tanks were filled with 32 parts per thousand (ppt) artificial seawater (Marine Art Hi, Tomita Pharmaceutical,
Japan), and placed in a 25 °C temperature-controlled room of the Aquaculture Biology
Laboratory, Nagasaki University, Japan. A spherical aerator (5 cm in diameter; 100
ml/min aeration rate) was placed at the bottom center of each tank to generate water flow.
Light intensity at the water surface was 2000 lux with a photoperiod of 24L:0D to
decrease the sinking syndrome that occurs in PBT larvae during dark periods (Nakagawa
et al., 2011; Tanaka et al., 2009; Takashi et al., 2006).

We followed the PBT larval rearing procedure described by Tanaka et al. (2018), who 99 successfully reared PBT larvae for 7 days dph in 200-1 tanks under static conditions (no 100 water exchange). Heavy mortality has been observed within 10 dph in the PBT mass 101 102 culture process due to the sinking syndrome, and the percentage of sinking PBT larvae on the tank bottom has been shown to peak at around 5 dph (Tanaka et al. 2009). We thus 103 104 decided on a rearing period of 8 dph. Fertilized eggs of PBT were obtained from Seikai 105 National Fisheries Research Institute, and were transported to the Aquaculture Biology 106 Laboratory, Nagasaki University, Japan, on 30 June 2018. Eggs were first transferred into a 100-l polycarbonate tank and larvae were kept until 2 dph in the same tank at 25 °C and 107 32 ppt. Larvae were distributed into each experimental tank at 10 individuals/l on 2 dph, 108 and reared until 8 dph under static conditions. Super Chlorella V12 (Chlorella Industry 109 Co., Fukuoka, Japan) was added to the experimental tanks as green water, and the density 110 was adjusted to 5×10^5 cells/ml once daily. Rotifers *Brachionus plicatilis* enriched with 111 Super Chlorella V12 were fed to larvae at 10 individuals/ml when the mouth opened (2 112 dph). Water samples to assess rotifer density were collected from 9 stations (3 ml for 113 each) in a vertical cross-section of CTs (Fig. 1(a)) and 27 stations in the quarter segments 114 of RTs (Fig. 1 (b)) using a pipet. Since the rotifer numbers in the experimental tanks 115

increased during the experimental period, we standardized the rotifer distribution in thetanks each sampling day using the following equations:

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deviation value at station x on day i =

rotifer density at station x-mean rotifer density on day i standard deviation of rotifer density on day i

On 8 dph, all surviving larvae in the experimental tanks were counted to calculate 120 the survival rate. Then, about 30 fish in each tank were anaesthetized with 200 ppm of 121 122 MS222 (Tricaine; Sigma-Aldrich) and observed under a dissecting microscope with 123 transmitted light to see whether the swimbladder was inflated by checking air bubbles in 124 the bladder. Larvae were then fixed with 5% formalin solution. Formalin-preserved fish 125 were individually measured for morphometric characteristics by a digital microscope (VH-6300; Keyence, Osaka, Japan), and then dried at 60 °C for 24 h for measurement of 126 the dry body weight by an ultra-micro balance (UMX2; Mettler Toledo, Columbus, OH, 127 128 USA).

Two-phase bubbly flow simulations were performed in the experimental tanks using 129 a dispersed flow model that was developed by Takakuwa et al. (2018). Its governing 130 equations are composed of the conservation laws of mass and momentum of liquid (water) 131 and gas (air bubble) phases, in which the effects of pressure gradient, drag and lift forces 132 acting on bubbles, gravitational acceleration and flow viscosity are taken into account. A 133 simplified marker and cell (SMAC) method was used to solve the governing equations. 134 For the liquid phase, the free surface was assumed to be flat, and a no-slip boundary 135 condition was used. On the other hand, an outflow condition was given for the gas phase 136 at the free surface. As boundary conditions on the wall surface of tanks, a no-slip 137 138 condition was given for the liquid phase, while a slip condition was given for the gas phase. An air inlet (square with a side length of 22 mm; aeration rate, 100 ml/min) was 139

140	set at the center of the bottom surface. The diameter of a bubble was set to 2.0 mm. Flow
141	simulations were performed for 450 s, and averaged flow fields for the last 150 s are
142	discussed in this research.
143	Physical environmental parameters during the experiments were as follows: water
144	temperature 24.3–24.8 °C; salinity 32.1–32.2 ppt; dissolved oxygen 6.2 mg/l; pH 7.94–
145	7.96; and ammonia (NH ₃ -N) 0.18–0.19 mg/l.

146 2.1 Statistical analysis

Differences in the survival, growth and swimbladder inflation rates of larvae between tanks were determined using either Student's *t*-test or Mann-Whitney *U*-test after Shapiro-Wilk normality test. The rotifer distribution in tanks was standardized by the deviation value on day *i*, and determined by two-way ANOVA followed by Tukey HSD test. All analyses used R 3.4.1 software, and a 5% level of confidence was considered a significant difference.

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154 **3. Results**

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156 *3.1. Survival, growth and swimbladder inflation of larvae*

The hatching rate of fish eggs was 100%. The survival rate of PBT larvae at 8 dph in CTs (52.7±5.1%) was significantly higher than in RTs ($0.8\pm0.7\%$, p<0.01, t-test; Table 1). Neither standard length nor dry weight of larvae was significantly different between tank shapes (Table 1). Other morphological parameters of larvae at 8 dph were also not significantly different: total length (CT, 4.23 ± 0.26 mm; RT, 4.09 ± 0.20 mm; p=0.9111, ttest, n=3), body depth/standard length (0.18 ± 0.02 mm; 0.17 ± 0.02 mm; p=0.8526, t-test, n=3), head length/standard length (0.23 ± 0.01 mm; 0.24 ± 0.02 mm; p=0.0765, Mann-Whitney *U*-test, n=3) and eye diameter/standard length (0.11 ± 0.01 mm; 0.11 ± 0.01 mm; p=0.6667, Mann-Whitney *U*-test, n=3). The swimbladder inflation rate of larvae was not significantly different between CT and RT (Table 1).

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168 *3.2 Flow field in the experimental tank*

3-D visualizations of streamlines in the rearing tanks are shown in Fig. 2. In the case 169 of the CT, upward flows by the effect of air bubbles generated from the air stone radiated 170 outward in the vicinity of the water surface, and then downward flows were observed 171 172 along the sidewalls of the tank. A single-pair vortex system could be observed at arbitrary 173 central sections. In the case of the RT, the central upward flows radiated outward in the 174 same manner as the CT. Due to the effect of rectangular corners and the non-axisymmetric shape of the tank, however, a more complicated flow field was generated. Figure 3 175 176 compares cumulative area distributions of the tanks with respect to the flow velocity 177 magnitude obtained from the flow simulation results. Low-velocity regions in the RT 178 were larger than in the CT regardless of the increasing flow velocity. In Fig. 4, streamlines at the bottom regions (where water depth is more than 25 cm) are visualized, colored by 179 the flow velocity magnitude. In the CT, although low-velocity regions were observed 180 along the outside edge, most streamlines eventually moved toward the center of the tank, 181 which reverted to the upward flow from the air stone. In the RT, the flow velocity 182 magnitude at most bottom regions was larger than the CT, and the flow structures were 183 more complicated. Streamlines from both short sides of the rectangle collided in the 184 vicinity of the center of the long sides, creating a vortex at the upper side of Fig. 4(b), and 185 186 a large low-velocity area at the lower side of the figure.

188 *3.2 Rotifer distribution*

Rotifer density increased during the experimental period, reaching 54.7 individuals/ml in CT and 52.2 individuals/ml in RT on 8 dph (n=6). Rotifer distribution expressed as an average of deviation values was significantly higher at the edge of the tank wall on the bottom in the CT, and from the air stone to the tank wall on the bottom in the RT (p<0.05, Tukey HSD test, n=6; Fig. 5).

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195 **4. Discussion**

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197 4.1 Survival, growth and swimbladder inflation of PBT larvae

The present study examined whether the shape of small-scale larval-rearing tanks affects 198 199 the survival and growth of PBT larvae, together with the rotifer distribution in tanks. The survival rate of PBT larvae in CTs at 8 dph was about 50-fold higher than that in RTs. 200 Usually, better survival and growth of larvae occurs in large rearing tanks rather than in 201 202 smaller systems (Houde, 1972). However, the survival rate in this study (52.7%) in the 50-1 CT under a 24-h photoperiod was higher than that in the 500-1 CT of a previous study 203 204 at 7 dph under natural photoperiod with strong aeration during darkness (about 35%; Tanaka et al., 2018), whose protocol with static conditions was followed here. Survival 205 rates in mass-scale tanks at similar ages were also lower than this study: 19.3% in a 50 206 m^3 octagonal tank with a water pump system under a natural photoperiod at 8 dph (Tanaka 207 et al., 2009), and 20.3% in 30 m³ circular tanks with 1.7 l/min aeration rates in daytime 208 209 and stronger aeration rates (3.0 l/min) during the dark period at 8 dph under a natural

210 photoperiod (Kurata et al., 2014).

211 Moreover, the survival rate in the present study was comparable to that at 10 dph in 1 m³ cylindrical fiberglass tanks (22.2–42.3%) with 130 ml/min daytime aeration rates, and 212 1.2 l/min dark-period aeration rates under natural and artificial fluorescent lighting 213 214 (Kurata et al., 2012), as well as those at 10 dph in 500-l cylindrical polycarbonate tanks 215 (43.2-48.6%) with 300 ml/min daytime aeration rates and 900 ml/min dark-period aeration rates at 12L:12D (Nakagawa et al., 2011). Therefore, we propose that rearing 216 experiments of PBT larvae can be conducted in small-scale tanks in which the rearing 217 environment, such as water temperature and illumination, can be easily manipulated. 218

219 We did not find significant differences in growth between different rearing tank 220 shapes. Similar findings were reported in the seven-band grouper Epinephelus 221 septemfasciatus and devil stinger Inimicus japonicus, for which the rearing tank shapes 222 affected larval survival but not growth (Ruttanapornvareesakul et al., 2007). The growth 223 of PBT larvae at 8 dph in the present study (about 4.1 mm TL) appeared to be smaller 224 than that of larvae of the same age in previous studies (5.8–6.1 mm: Kurata et al., 2012, 2014). Growth measurements were conducted with formalin-fixed specimens in the 225 present study and fresh specimens in Kurata et al. (2012, 2014). If we assume 10% 226 shrinkage in the case of formalin-fixed larvae (Hay, 1982) to the previous studies (Kurata 227 et al., 2012, 2014), body size of our sample (4.1 mm) was still smaller than that of the 228 previous studies (5.2–5.5 mm). The inferior growth of PBT larvae in this study may have 229 been due to the smaller tank volume; thus, we should consider the larval density and water 230 exchange when applying small-scale tanks for PBT larviculture experiments. 231

Sinking syndrome of PBT larvae occurs because larvae with higher body density
than seawater sink to the bottom of the tank during dark periods due to low swimming

activity (Tanaka et al., 2009; Takashi et al., 2006). Swimbladder inflation failure is one of 234 the causes of sinking syndrome (Kurata et al., 2017, 2015, 2012; Ina et al., 2014; Woolley 235 and Qin, 2013), as the swimbladder controls the buoyancy of fish by reducing body 236 density relative to that of surrounding water (Taylor et al., 2010; Phleger, 1998). However, 237 Takashi et al. (2006) found that the body density of PBT larvae was higher than seawater 238 239 density during dark periods even in swimbladder-inflated larvae. In the present study, the swimbladder inflation rate varied among tanks but was not significantly different between 240 tank shapes. We presume that swimbladder inflation failure may not be the main cause of 241 sinking syndrome. These results may be in agreement with the present finding that the 242 survival rate in the CT was higher than that in the RT despite the same swimbladder 243 244 inflation rates between tank shapes. We could not conclusively determine whether swimbladder inflation is directly connected to the cause of sinking syndrome; additional 245 studies with more detailed observations of the diel movement of PBT larvae in the rearing 246 247 tank will be needed.

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249 4.2 Flow field in the cylindrical and rectangular tanks

Unfavorable flow in rearing tanks can cause mass mortality of marine fish larvae 250 (Sakakura et al., 2019; Shiotani et al., 2003; Yamaoka et al., 2000; Backhurst and Harker, 251 1988). Flow field structures in tanks differ by tank size and shape (Sakakura et al., 2019; 252 Moore and Prange, 1994). CTs have an axisymmetrical flow field pattern (Sumida et al., 253 2013), and the flow field provides a uniform current environment and facilitates the 254 elimination of biosolids from the tank bottom (Masaló and Oca, 2016; Oca and Masaló, 255 2013; Timmons et al., 1998). In the case of RTs, 3-D complicated flow fields and low-256 flow areas were observed in this study, confirming the findings of a previous study 257

(Takakuwa et al., 2018). Low-velocity areas were larger in the RT, as shown in Fig. 3. 258 Moreover, these low-flow areas and the eddy at the tank bottom coincided with the areas 259 where rotifers were distributed at high density. Thus, the low-flow areas in RTs may be 260 261 larger at the bottom than in CTs, leading to the sinking syndrome of PBT larvae because low velocities and poor mixing of water in rectangular tanks lead to the creation of 262 263 stagnate areas, causing the accumulation of biosolids on the tank bottom (Oca and Masalò, 2007). These low-flow areas may have negative effects on larviculture (Sakakura et al., 264 2019). 265

The advantage of numerical modeling of the flow field in a larviculture tank is 266 that we can visualize the field in the rearing tank without a flow meter or intensive labor, 267 and that one established model can be expanded to similarly shaped tanks with different 268 269 water volumes. Thus, the flow field in similar tank shapes can be easily estimated and the model can help in designing the number and location of aerators and water inlets for the 270 271 larviculture tank. Our results also demonstrated that comparison of rotifer densities at 272 various sites in a rearing tank could approximately predict the low-flow areas that will cause the sinking syndrome of marine fish larvae. 273

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In conclusion, the flow field in different larval rearing tank shapes affected the survival of PBT larvae in our experiments. The present study demonstrated that flow field patterns in small-scale CTs (50-1) at AR=1.3 are more feasible for the survival of PBT larviculture experiments than those in RTs, and that improvement of aerators beyond a single air stone to decrease low-flow areas at the tank bottom should be developed for RTs.

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417 Figure captions

418	Fig. 1. Sites for rotifer distribution in (a) a cylindrical tank, and (b) a rectangular tank.
419	One air stone was set at the center of the tank bottom.
420	
421	Fig. 2. Three-dimensional streamlines predicted in this study in (a) a cylindrical tank (ø
422	46 cm \times 29 cm depth), and (b) a rectangular tank (60×30×28 cm depth) with an
423	aerator at the center of the bottom with 100 ml/min aeration.
424	
425	Fig. 3. Cumulative area (%) of the velocity magnitude (< x mm/s) between the tanks
426	applied in this study. For instance, the water mass having a velocity between 0–10
427	mm/s occupied 40% and 65% of total water volume in the CT and RT in this study,
428	respectively.
429	
430	Fig. 4. Visualization of streamlines at bottom regions of (a) a cylindrical tank (ø 46 cm),
431	and (b) a rectangular tank (60×30 cm) in this study. An air stone was located at the
432	center of each graph.
433	
434	Fig. 5. Rotifer distribution (a) at half-cross section in the CT, and (b) in the quadrisection
435	in the RT. Values are average of deviation values during the culture period (n=6,
436	a>b>c>d, Tukey HSD, <i>p</i> <0.05).

1 **Table. 1.** Survival, growth and swimbladder inflation rates of *T. orientalis* larvae at 8 dph

Tank	n	Survival	Standard	Dry weight	Swimbladder inflation
Tunk	п	(%) *	length (mm)	(µg)	(%)
Cylindrical	3	52.7 ± 5.1	4.06±0.25	95.1±17.6	16.5 ± 14.5 (n=30)
Rectangular	3	0.8 ± 0.7	3.91±0.20	67.7±10.9	$56.9 \pm 37.4 \ (n=1-8)$

2 in tanks of different shapes

3 Results are mean values \pm SD. The asterisk indicates a significant difference by *t*-test (*p*

4 < 0.01).



Fig. 1.







Fig. 3.





Fig. 5.

(a)



